# Tilt Sensing Using Linear Accelerometers 

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## INTRODUCTION

This application note explains the importance of understanding how to acquire a reliable and accurate tilt reading for accelerometer applications by comparing the advantages and disadvantages of various tilt measurement techniques. Accelerometers used for tilt sensing require high resolution to meet the demands of many new emerging applications such as tilt enabled computer mouse/pointers, motion enabled video game solutions and PDA-cell phone/ mp3 player screen navigation.

The overall benefit of the accelerometer for tilting applications used in PDAs for screen navigations is a new method to view, scroll, select and move with a minimum number of buttons required. This concept affords a PDA with a larger screen area for viewing. Navigation through menus is made easier with the ability to make selections based on tilt. The choices are highlighted and then can be selected either by using a physical "execute" button on the PDA or by using click or double click tap detection of the accelerometer. The user can make selections in a menu driven environment this way. Also the accelerometer can also be used to sense the tilt of the PDA to change from landscape to portrait using gravity to change the screen orientation for viewing.

Interactive video games are becoming increasingly popular. Accelerometers are used to detect the tilting motions of the joystick for the game.This has created games where the user can feel more immersed in the game.

Tilt is a static measurement. The force of gravity is used as an input to determine the orientation of an object calculating the degree of tilt.The accelerometer will experience acceleration in the range from -1 g to +1 g through $180^{\circ}$ of tilt.

$$
1 \mathrm{~g}=-9.8 \mathrm{~m} / \mathrm{s}^{2}
$$

## OG OFFSET CALIBRATION

Accuracy and repeatability is a general concern for nearly all accelerometer applications. The accuracy of the tilt measurement can be improved by using a $0 g$-offset calibration technique to compensate for offset errors. Refer to Freescale application note AN3447, "Implementing Auto-Zero

Calibration Technique for Accelerometers." Even though the offset is trimmed, offset can shift due to packaging stresses, aging and external mechanical stresses due to mounting and orientation. This results in offset calibration error. It is important to implement a Og calibration routine for the accelerometer to compensate for the 0 g offset.

## MEASUREMENT TECHNIQUES

This section discusses the different ways to implement tilt comparing different ways to measure the corresponding angle from the acceleration output.

## Measuring Tilt using One Axis

In the case of a dual-axis accelerometer (XY) mounted perpendicular to gravity the tilt algorithm is limited to one axis of sensitivity. As shown in Figure 1 the accelerometer is tilted along the X -axis. The Y -axis remains at Og output throughout the full rotation of the $X$-axis in this case.


Figure 1. Dual-Axis Accelerometer with One Axis of Tilt
If one axis ( X -axis) is used to calculate the tilted angle of the accelerometer the following trigonometry relationship is used:

$$
V_{\text {OUTX }}=V_{\text {OFF }}+S \times \sin \theta
$$

Where: $\mathrm{V}_{\text {OUTX }}$ is the voltage output from the X -axis of the accelerometer, $\mathrm{V}_{\text {OFF }}$ is the offset voltage, and S is the sensitivity of the accelerometer.

The acceleration output on the X -axis due to gravity is equal to the following:

$$
A_{X}=\frac{V_{\text {OUTX }}-V_{\text {OFF }}}{S}
$$

In order to solve for the angle of tilt the equation becomes the following:

$$
\theta=\sin ^{-1}\left(A_{x}\right)
$$



Figure 2. Accelerometer Output ( $\mathbf{g}$ 's) Tilting from $-90^{\circ}$ to $+90^{\circ}$ with a One Axis Measurement

This graph shows the output in g's of the accelerometer as it tilts from $-90^{\circ}$ to $+90^{\circ}$. Notice that the tilt sensitivity diminishes between $-90^{\circ}$ and $-45^{\circ}$ and between $+45^{\circ}$ to $+90^{\circ}$. This resolution problem between these values makes this method of calculating the angle of tilt inaccurate when the accelerometer output is near the +1 g or -1 g range. A dual-axis accelerometer horizontally mounted would be limited by this method of calculating tilt and would not be accurate over a $360^{\circ}$ rotation. It would only be useful for angle measurements between $-45^{\circ}$ to $+45^{\circ}$ of tilt.

Another disadvantage of the single axis measurement tilt technique is that it is impossible to know the difference between two tilt angles that result in the same sensor output. The output is a sine function, so for example it would be impossible to know from a 0.5 g output reading if the accelerometer was tilted $30^{\circ}$ or $150^{\circ}$ by looking at the accelerometer output. One would have to be aware of the correct orientation of the accelerometer and have a sense for the quadrant of tilt. This disadvantage is overcome by using a two axis measurement tilt technique and is explained in the next section.

## Measuring Tilt using a Two Axis Solution

The resolution problems and tilt orientation difficulties can be addressed by mounting the accelerometer vertically so that the Y -axis is parallel to gravity, or by using a tri-axis accelerometer using at least 2 of the 3 axis. Using more than one axis to calculate tilt produces a more accurate solution.


Figure 3. Using a (Dual- or Tri-Axis) Accelerometer with Two Axes for Measuring Tilt


Figure 4. Sine Function of the $X$ Output and Cosine Function of the Y Output

The graph above shows that when using a two axis solution the component due to gravity on the X-axis follows the sine function while the component due to gravity acting on the Y-axis follows the cosine function. Notice that the tilt sensitivity (slope of the line) in the $X$-direction is at its maximum while the Y-sensitivity is at its minimum and visa versa. Therefore the maximum tilt sensitivity can be maintained if both the $X$ and the $Y$ outputs are combined.

Table 1 displays $360^{\circ}$ of tilt with the acceleration output of the $X$ component and $Y$ components due to gravity. Also the change in gravity with the change in angle is analyzed through the full rotation for both components. The two sensitivities are combined which results in a constant output of $17.45 \mathrm{mg} /{ }^{\circ}$.

Table 1. Tilt using the $X$ and $Y$-axis

| Angle ( ${ }^{\circ}$ ) | $A_{X}$ (g's) | $\begin{gathered} \operatorname{dg} / \mathrm{dDeg} A_{X} \\ \mathrm{TS} \mathrm{~S}_{\mathrm{X}}\left(\mathrm{mg} /^{\circ}\right) \end{gathered}$ | $A_{Y}\left(g^{\prime} \mathrm{s}\right)$ | $\begin{gathered} \text { dg/dDeg } A_{Y} \\ T S_{Y}\left(m g /^{\circ}\right) \end{gathered}$ | $\begin{gathered} \text { sqrt(TS } \mathrm{N}_{\chi} \wedge_{2}^{\wedge}(\mathrm{mg}) \end{gathered}$ | $\underset{(g)}{\operatorname{sqrt}\left(A_{X}^{\wedge}\right)^{\wedge}+A_{Y}{ }^{\wedge} 2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0.000 | 17.452 | 1.000 | -0.152 | 17.45 | 1.00 |
| 30 | 0.500 | 15.038 | 0.866 | -8.858 | 17.45 | 1.00 |
| 60 | 0.866 | 8.594 | 0.500 | -15.190 | 17.45 | 1.00 |
| 90 | 1.000 | -0.152 | 0.000 | -17.452 | 17.45 | 1.00 |
| 120 | 0.866 | -8.858 | -0.500 | -15.038 | 17.45 | 1.00 |
| 150 | 0.500 | -15.190 | -0.866 | -8.594 | 17.45 | 1.00 |
| 180 | 0.000 | -17.452 | -1.000 | 0.152 | 17.45 | 1.00 |
| 210 | -0.500 | -15.038 | -0.866 | 8.858 | 17.45 | 1.00 |
| 240 | -0.866 | -8.594 | -0.500 | 15.190 | 17.45 | 1.00 |
| 270 | -1.000 | 0.152 | 0.000 | 17.452 | 17.45 | 1.00 |
| 300 | -0.866 | 8.858 | 0.500 | 15.038 | 17.45 | 1.00 |
| 330 | -0.500 | 15.190 | 0.866 | 8.594 | 17.45 | 1.00 |

## Basic Trigonometry



Figure 5. Basic Trigonometry
The acceleration in the $X$-axis in Table 1 is calculated by the following equation:

$$
A_{X}=\sin \theta
$$

The acceleration on the Y -axis is calculated with:

$$
A_{Y}=\cos \theta
$$

If the combination of the $X$ acceleration and the $Y$ acceleration is used:

$$
\frac{\mathrm{A}_{X}}{\mathrm{~A}_{Y}}=\tan \theta
$$

The tilt sensitivity equation $\mathrm{mg} /{ }^{\circ}$ was calculated by taking the difference between the acceleration output between 1 degree at that point. For example, the tilt sensitivity at $15^{\circ}$ is calculated by the following:

$$
\sin (16)-\sin (15)=16.818
$$

The $Y$-axis is $90^{\circ}$ from the $X$-axis and therefore it makes sense that the $Y$-axis experiences a 1 g acceleration while the

X -axis experiences a 0 g acceleration. The combined acceleration is always 1 g .

$$
A=\sqrt{A_{X}^{2}+A_{Y}^{2}}=1 g
$$

The sensor is most responsive to changes in tilt when the sensitive axis is perpendicular to the force of gravity. When perpendicular to the force of gravity the accelerometer experiences approximately 17.45 mg per degree tilt. It is least responsive when the sensitive axis is parallel to the force of gravity in the +1 g or -1 g orientation, with a responsiveness of only 0.15 mg per degree of tilt. This is clearly displayed in Figure 6 where the absolute value of the tilt sensitivity was taken. As the X -axis is at its minimum tilt sensitivity the Y -axis is at its maximum tilt sensitivity. By combining the $X$ and Y -axis solving for the tilt angle using arctan ( $\mathrm{A}_{\mathrm{X}} / \mathrm{A}_{Y}$ ), a constant tilt sensitivity of 17.45 mg can be maintained through a $360^{\circ}$ rotation.


Figure 6. Tilt Sensitivity versus Tilt Angle

## Quadrant Orientation



Figure 7. Quadrants of a 360 Degree Rotation
It is important to know the sign of the $X$ and $Y$ accelerations to determine the quadrant of tilt that is applicable because the outputs from the first and third quadrant will be the same and the outputs from the second and fourth quadrant will also be the same. For example $\tan (45)=1$ and $\tan (225)=1$. When taking the arctan of a positive value the tilt angle is in either the first or third quadrant. Knowing the sign of $A_{X}$ and $A_{Y}$ will determine exactly which quadrant. When taking the arctan of a negative value the tilt angle is in either the second or fourth quadrant. Knowing the sign of $A_{X}$ and $A_{Y}$ will determine exactly which quadrant the accelerometer is tilting through.

$$
\begin{aligned}
& \text { If in Quadrant } 1=\arctan \left(A_{X} / A_{Y}\right) \\
& \text { If in Quadrant } 2=\arctan \left(A_{X} / A_{Y}\right)+180 \\
& \text { If in Quadrant } 3=\arctan \left(A_{X} / A_{Y}\right)+180 \\
& \text { If in Quadrant } 4=\arctan \left(A_{X} / A_{Y}\right)+360
\end{aligned}
$$

## Measuring Tilt using a Three Axis Solution

In order to define the angles of the accelerometer in three dimensions the pitch, roll and theta are sensed using all three outputs of the accelerometer. Pitch ( $\rho$ ) is defined as the angle of the $X$-axis relative to ground. Roll $(\varphi)$ is defined as the angle of the $Y$-axis relative to the ground. Theta $(\theta)$ is the angle of the $Z$ axis relative to gravity.


Figure 8. Three Axis for Measuring Tilt

$$
\begin{aligned}
& \rho=\arctan \left(\frac{A_{X}}{\sqrt{A_{Y}^{2}+A_{Z}^{2}}}\right) \\
& \phi=\arctan \left(\frac{A_{Y}}{\sqrt{A_{X}^{2}+A_{Z}^{2}}}\right) \\
& \theta=\arctan \left(\frac{\sqrt{A_{X}^{2}+A_{Y}^{2}}}{A_{Z}}\right)
\end{aligned}
$$

Now the acceleration due to gravity on the X -axis, $Y$-axis and $Z$-axis are combined. The resultant sum of the accelerations from the three axes is equal to 1 g when the accelerometer is static.

$$
\sqrt{A_{X}^{2}+A_{Y}^{2}+A_{Z}^{2}}=1 g
$$

## A/D Converter Resolution Limitations

Discrete values are used when the signal is digitized and therefore the resolution is limited by the number of bits in the A/D converter. Table 2 displays the 8 -bit A/D converter values for the $X$ and $Z$-axis assuming an ideal rotation about the y axis.

The 3.3 V supply voltage is divided by $255\left(2^{8}-1\right)$ steps from the A/D converter. This value is divided by the sensitivity of $0.8 \mathrm{~V} / \mathrm{g}$ to solve for the acceleration due to gravity at each step.

$$
\frac{3.3 \mathrm{~V}}{255 \times 0.8 \mathrm{mV} / \mathrm{g}}=16.176 \mathrm{mg}
$$

Therefore each increasing bit will account for an additional 16.176 mg .

From Table 2 it can be seen that a single axis solution will produce a decreasing resolution as the device is tilted from $0^{\circ}$ to $90^{\circ}$, but a two axis solution will produce a fairly steady resolution throughout the entire tilt range.

The angle calculation based on acceleration of a single axis is the following:

$$
\theta=\sin ^{-1}\left(A_{x}\right)
$$

The resolution goes from 0.927 degrees to 9.332 , which is unacceptable for a tilt application. The resolution gets increasingly worse through the tilt.

The angle calculation based on acceleration of two axes is the following:

$$
\theta=\tan ^{-1}\left(\frac{\mathrm{~A}_{x}}{\mathrm{~A}_{\mathrm{z}}}\right)
$$

The resolution is between $0.748^{\circ}-1.317^{\circ}$ throughout the entire tilt range. Again this shows the improved accuracy of using two axes to calculate tilt. Figure 6 displays the comparison of these two methods using the 8-bit A/D converter.
NOTE: The same analysis applies for angles from $91^{\circ}$ to $360^{\circ}$ in the other three quadrants.
Using a 10-bit A/D converter the 3.3 V supply voltage is divided by $1023\left(2^{10}-1\right)$ steps from the A/D converter. This value is then divided by the sensitivity of $0.8 \mathrm{~V} / \mathrm{g}$ to solve for the acceleration due to gravity at each step.

$$
\frac{3.3 \mathrm{~V}}{1023 \times 0.8 \mathrm{mV} / \mathrm{g}}=4.032 \mathrm{mg}
$$

Using a 10-bit A/D converter with a 2 axis solution the resolution is between 0.171 and 0.327 throughout the tilt range, while the 1 axis solution resolution starts out at 0.231 at $0^{\circ}$ and increases to 5.147 as it approaches $90^{\circ}$. A higher resolution is achievable with a bigger A/D converter. The
comparison using the 10-bit A/D converter is shown in Figure 10.


Figure 9. Tilt Resolution for a One or Two axis Tilt Algorithm Using an 8-Bit A/D Converter


Figure 10. Tilt Resolution for a One or Two Axis Tilt Algorithm Using a 10-Bit A/D Converter

Table 2. A/D converter values for $A_{X}$ and $A_{Z}$ for tilt from $0^{\circ}$ to $90^{\circ}$

| AID $\mathrm{A}_{\mathrm{X}}$ | Ax-g's | A/D $\mathrm{Z}_{\mathbf{z}}$ | Az-g's | Angle 1-Axis | Angle 2-Axes | Resolution 1-Axis | Resolution 2=Axis |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 128 | 0.0000 | 190 | 1.0029 | 0.0000 | 0.0000 | 0.9269 | 0.9240 |
| 129 | 0.0162 | 190 | 1.0029 | 0.9269 | 0.9240 | 0.9269 | 0.9240 |
| 130 | 0.0324 | 190 | 1.0029 | 1.8540 | 1.8476 | 0.9271 | 0.9236 |
| 131 | 0.0485 | 190 | 1.0029 | 2.7816 | 2.7702 | 0.9276 | 0.9226 |
| 132 | 0.0647 | 190 | 1.0029 | 3.7100 | 3.6914 | 0.9283 | 0.9212 |
| 133 | 0.0809 | 190 | 1.0029 | 4.6393 | 4.6106 | 0.9293 | 0.9193 |
| 134 | 0.0971 | 190 | 1.0029 | 5.5698 | 5.5275 | 0.9305 | 0.9169 |
| 135 | 0.1132 | 189 | 0.9868 | 6.5018 | 6.5463 | 0.9320 | 1.0188 |
| 136 | 0.1294 | 189 | 0.9868 | 7.4356 | 7.4716 | 0.9338 | 0.9253 |
| 137 | 0.1456 | 189 | 0.9868 | 8.3713 | 8.3929 | 0.9357 | 0.9214 |
| 138 | 0.1618 | 189 | 0.9868 | 9.3093 | 9.3099 | 0.9380 | 0.9170 |
| 139 | 0.1779 | 189 | 0.9868 | 10.2499 | 10.2222 | 0.9405 | 0.9122 |
| 140 | 0.1941 | 189 | 0.9868 | 11.1932 | 11.1292 | 0.9433 | 0.9070 |
| 141 | 0.2103 | 188 | 0.9706 | 12.1396 | 12.2251 | 0.9464 | 1.0959 |
| 142 | 0.2265 | 188 | 0.9706 | 13.0894 | 13.1340 | 0.9498 | 0.9089 |
| 143 | 0.2426 | 188 | 0.9706 | 14.0428 | 14.0362 | 0.9535 | 0.9022 |
| 144 | 0.2588 | 188 | 0.9706 | 15.0003 | 14.9314 | 0.9574 | 0.8952 |
| 145 | 0.2750 | 187 | 0.9544 | 15.9620 | 16.0736 | 0.9617 | 1.1422 |
| 146 | 0.2912 | 187 | 0.9544 | 16.9284 | 16.9661 | 0.9664 | 0.8926 |
| 147 | 0.3074 | 187 | 0.9544 | 17.8998 | 17.8503 | 0.9714 | 0.8842 |
| 148 | 0.3235 | 187 | 0.9544 | 18.8765 | 18.7258 | 0.9767 | 0.8755 |
| 149 | 0.3397 | 186 | 0.9382 | 19.8590 | 19.9037 | 0.9825 | 1.1780 |
| 150 | 0.3559 | 186 | 0.9382 | 20.8475 | 20.7723 | 0.9886 | 0.8685 |
| 151 | 0.3721 | 185 | 0.9221 | 21.8426 | 21.9745 | 0.9951 | 1.2023 |
| 152 | 0.3882 | 185 | 0.9221 | 22.8447 | 22.8337 | 1.0021 | 0.8591 |
| 153 | 0.4044 | 185 | 0.9221 | 23.8543 | 23.6821 | 1.0095 | 0.8484 |
| 154 | 0.4206 | 184 | 0.9059 | 24.8717 | 24.9048 | 1.0175 | 1.2227 |
| 155 | 0.4368 | 184 | 0.9059 | 25.8976 | 25.7407 | 1.0259 | 0.8359 |
| 156 | 0.4529 | 183 | 0.8897 | 26.9325 | 26.9802 | 1.0349 | 1.2395 |
| 157 | 0.4691 | 183 | 0.8897 | 27.9770 | 27.8015 | 1.0445 | 0.8212 |

AN3461

Table 2. A/D converter values for $A_{X}$ and $A_{Z}$ for tilt from $0^{\circ}$ to $90^{\circ}$ (continued)

| A/D $A_{x}$ | Ax-g's | A/D $\mathrm{A}_{\mathbf{z}}$ | Az-g's | Angle 1-Axis | Angle 2-Axes | Resolution 1-Axis | $\begin{aligned} & \text { Resolution } \\ & 2=\text { Axis } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 158 | 0.4853 | 182 | 0.8735 | 29.0317 | 29.0546 | 1.0547 | 1.2531 |
| 159 | 0.5015 | 181 | 0.8574 | 30.0973 | 30.3236 | 1.0656 | 1.2690 |
| 160 | 0.5176 | 181 | 0.8574 | 31.1746 | 31.1225 | 1.0772 | 0.7989 |
| 161 | 0.5338 | 180 | 0.8412 | 32.2642 | 32.3998 | 1.0896 | 1.2774 |
| 162 | 0.5500 | 180 | 0.8412 | 33.3670 | 33.1785 | 1.1029 | 0.7787 |
| 163 | 0.5662 | 179 | 0.8250 | 34.4840 | 34.4608 | 1.1170 | 1.2823 |
| 164 | 0.5824 | 178 | 0.8088 | 35.6162 | 35.7539 | 1.1322 | 1.2931 |
| 165 | 0.5985 | 178 | 0.8088 | 36.7646 | 36.5014 | 1.1484 | 0.7476 |
| 166 | 0.6147 | 177 | 0.7926 | 37.9306 | 37.7939 | 1.1659 | 1.2925 |
| 167 | 0.6309 | 176 | 0.7765 | 39.1153 | 39.0939 | 1.1847 | 1.2999 |
| 168 | 0.6471 | 175 | 0.7603 | 40.3202 | 40.3999 | 1.2050 | 1.3060 |
| 169 | 0.6632 | 174 | 0.7441 | 41.5471 | 41.7108 | 1.2269 | 1.3109 |
| 170 | 0.6794 | 173 | 0.7279 | 42.7977 | 43.0251 | 1.2506 | 1.3143 |
| 171 | 0.6956 | 172 | 0.7118 | 44.0741 | 44.3415 | 1.2764 | 1.3164 |
| 172 | 0.7118 | 171 | 0.6956 | 45.3787 | 45.6585 | 1.3046 | 1.3171 |
| 173 | 0.7279 | 170 | 0.6794 | 46.7141 | 46.9749 | 1.3354 | 1.3164 |
| 174 | 0.7441 | 169 | 0.6632 | 48.0834 | 48.2892 | 1.3693 | 1.3143 |
| 175 | 0.7603 | 168 | 0.6471 | 49.4901 | 49.6001 | 1.4068 | 1.3109 |
| 176 | 0.7765 | 167 | 0.6309 | 50.9386 | 50.9061 | 1.4484 | 1.3060 |
| 177 | 0.7926 | 166 | 0.6147 | 52.4336 | 52.2061 | 1.4950 | 1.2999 |
| 178 | 0.8088 | 165 | 0.5985 | 53.9811 | 53.4986 | 1.5476 | 1.2925 |
| 178 | 0.8088 | 164 | 0.5824 | 53.9811 | 54.2461 | 1.5476 | 0.7476 |
| 179 | 0.8250 | 163 | 0.5662 | 55.5885 | 55.5392 | 1.6073 | 1.2931 |
| 180 | 0.8412 | 162 | 0.5500 | 57.2646 | 56.8215 | 1.6761 | 1.2823 |
| 180 | 0.8412 | 161 | 0.5338 | 57.2646 | 57.6002 | 1.6761 | 0.7787 |
| 181 | 0.8574 | 160 | 0.5176 | 59.0207 | 58.8775 | 1.7561 | 1.2774 |
| 181 | 0.8574 | 159 | 0.5015 | 59.0207 | 59.6764 | 1.7561 | 0.7989 |
| 182 | 0.8735 | 158 | 0.4853 | 60.8714 | 60.9454 | 1.8507 | 1.2690 |
| 183 | 0.8897 | 157 | 0.4691 | 62.8363 | 62.1985 | 1.9649 | 1.2531 |
| 183 | 0.8897 | 156 | 0.4529 | 62.8363 | 63.0198 | 1.9649 | 0.8212 |
| 184 | 0.9059 | 155 | 0.4368 | 64.9424 | 64.2593 | 2.1061 | 1.2395 |
| 184 | 0.9059 | 154 | 0.4206 | 64.9424 | 65.0952 | 2.1061 | 0.8359 |
| 185 | 0.9221 | 153 | 0.4044 | 67.2289 | 66.3179 | 2.2866 | 1.2227 |
| 185 | 0.9221 | 152 | 0.3882 | 67.2289 | 67.1663 | 2.2866 | 0.8484 |
| 185 | 0.9221 | 151 | 0.3721 | 67.2289 | 68.0255 | 2.2866 | 0.8591 |
| 186 | 0.9382 | 150 | 0.3559 | 69.7573 | 69.2277 | 2.5283 | 1.2023 |
| 186 | 0.9382 | 149 | 0.3397 | 69.7573 | 70.0963 | 2.5283 | 0.8685 |
| 187 | 0.9544 | 148 | 0.3235 | 72.6329 | 71.2742 | 2.8756 | 1.1780 |
| 187 | 0.9544 | 147 | 0.3074 | 72.6329 | 72.1497 | 2.8756 | 0.8755 |
| 187 | 0.9544 | 146 | 0.2912 | 72.6329 | 73.0339 | 2.8756 | 0.8842 |
| 187 | 0.9544 | 145 | 0.2750 | 72.6329 | 73.9264 | 2.8756 | 0.8926 |
| 188 | 0.9706 | 144 | 0.2588 | 76.0694 | 75.0686 | 3.4366 | 1.1422 |
| 188 | 0.9706 | 143 | 0.2426 | 76.0694 | 75.9638 | 3.4366 | 0.8952 |
| 188 | 0.9706 | 142 | 0.2265 | 76.0694 | 76.8660 | 3.4366 | 0.9022 |
| 188 | 0.9706 | 141 | 0.2103 | 76.0694 | 77.7749 | 3.4366 | 0.9089 |
| 189 | 0.9868 | 140 | 0.1941 | 80.6678 | 78.8708 | 4.5983 | 1.0959 |

## AN3461

Table 2. AID converter values for $A_{X}$ and $A_{Z}$ for tilt from $0^{\circ}$ to $90^{\circ}$ (continued)

| A/D A $\mathbf{X}^{\prime}$ | Ax- g's | A/D A | Az-g's | Angle <br> 1-Axis | Angle <br> 2-Axes | Resolution <br> 1-Axis | Resolution <br> 2=Axis |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 189 | 0.9868 | 139 | 0.1779 | 80.6678 | 79.7778 | 4.5983 | 0.9070 |
| 189 | 0.9868 | 138 | 0.1618 | 80.6678 | 80.6901 | 4.5983 | 0.9122 |
| 189 | 0.9868 | 137 | 0.1456 | 80.6678 | 81.6071 | 4.5983 | 0.9170 |
| 189 | 0.9868 | 136 | 0.1294 | 80.6678 | 82.5284 | 4.5983 | 0.9214 |
| 189 | 0.9868 | 135 | 0.1132 | 80.6678 | 83.4537 | 4.5983 | 0.9253 |
| 190 | 1.0029 | 134 | 0.0971 | 90.0000 | 84.4725 | 9.3322 | 1.0188 |
| 190 | 1.0029 | 133 | 0.0809 | 90.0000 | 85.3894 | 9.3322 | 0.9169 |
| 190 | 1.0029 | 132 | 0.0647 | 90.0000 | 86.3086 | 9.3322 | 0.9193 |
| 190 | 1.0029 | 131 | 0.0485 | 90.0000 | 87.2298 | 9.3322 | 0.9212 |
| 190 | 1.0029 | 130 | 0.0324 | 90.0000 | 88.1524 | 9.3322 | 0.9226 |
| 190 | 1.0029 | 129 | 0.0162 | 90.0000 | 89.0760 | 9.3322 | 0.9236 |
| 190 | 1.0029 | 128 | 0.0000 | 90.0000 | 90.0000 | 9.3322 | 0.9240 |

AN3461

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